

# Mobile Campimetry

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## Abstract

Campimetry is an important test to detect and monitor central and peripheral ocular dysfunctions, which might indicate the existence of serious conditions such as glaucoma, or the occurrence of strokes or brain tumors. Commercially-available campimeters are expensive and lack portability. We present a portable, low-cost, easy-to-manufacture smartphone-based campimeter. We evaluated our prototype in a user-study, which has shown that its results are consistent with the ones obtained with the Humphrey Field Analyzer - HFA II-i campimeter, with a Pearson correlation coefficient above 0.98 for all sampling positions on the visual field. Moreover, its reproducibility is also comparable to the Humphrey campimeter. Given its portability and low cost, our mobile campimeter provides a promising alternative for patient screening in schools and community health centers, as well as for visual evaluation of patients with mobility restrictions, for keeping

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track of the visual field at home, and for use in communities with limited access to medical services.

*Keywords:* Campimetry, Smartphone-based Campimeter, Visual Acuity, Vision Health.

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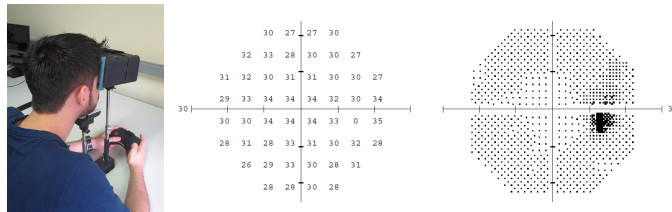


Figure 1: Our mobile campimeter. (left) Prototype during a visual field evaluation. (center) Minimum perceived intensities (in dB) computed by our campimeter and (right) its graphical representation (blind spot shown as a dark spot). A complete report example is shown in Appendix B.

## 1. Introduction

*Campimetry*, also known as *perimetry*, is an important test to detect and monitor central and peripheral ocular disfunctions. These might indicate the existence of serious conditions such as glaucoma, or the occurrence of strokes or brain tumors, which pose serious threats to one’s health, and may dramatically affect the person’s quality of life. Glaucoma, for instance, the leading cause of irreversible blindness, damages the optic nerve and often manifests itself as a silent disease. Without proper treatment, it may lead to blindness in just a few years [1]. Current estimates indicate that the worldwide prevalence of glaucoma in the population aged 40-80 years is approximately 3.54%, affecting over 64 million individuals, and should reach 76 million by

2020, and 111.8 million by 2040 [2]. Surprisingly, more than half of the patients suffering from glaucoma in developed countries are unaware of their condition. The situation is even more critical in underdeveloped countries.

Campimetry is a psychophysical test that checks the subject’s perception of stimuli across the visual field. One eye at time, the patient should acknowledge each visual stimulus by pressing a button. The resulting maps reporting the minimum perceived intensities across the visual field are used by doctors along with other data (such as intraocular pressure or images of the optical nerve structure and the retina) for diagnosis.

The first concepts of computational campimetry appeared around 1970 [3] and provided the basis for current devices. Modern campimeters are still big and expensive, costing tens of thousands of dollars and found almost exclusively in ophthalmology clinics. Their lack of portability and high cost has prevented their widespread use as screening devices for ocular disfunctions. The availability of a portable, low-cost campimeter could change this situation, with the potential to significantly reduce the number of cases of avoidable blindness.

*We present a smartphone-based campimeter* designed to fulfill such needs. We have validated our prototype by performing a user study with 20 participants, who performed visual field evaluation both on our prototype and on a modern commercial campimeter (the Humphrey Field Analyzer - HFA II-i). We compared the subjects’ evaluations using statistical tools for perimetry examination [4], and show that the results produced by our prototype are consistent with the ones obtained with the HFA II-i campimeter, with a Pearson correlation coefficient above 0.98 for all sampling points on the vi-

1 sual field. Moreover, its reproducibility is also comparable to the one of the  
2 HFA II-i using the SITA Fast algorithm. Thus, our mobile campimeter pro-  
3 vides a promising alternative for patient screening in schools, organizations,  
4 and communities with limited access to medical services, as well as for visual  
5 evaluation of patients with reduced mobility. Fig. 1 illustrates the use of our  
6 mobile campimeter prototype in one of its possible configurations, and shows  
7 examples of its reports.

8 The **contributions** of our work include:

- 9 • The design and demonstration of a portable, low-cost, smartphone-  
10 based campimeter (Section 3). Our prototype obtains results compa-  
11 rable to the ones obtained with commercial perimeters. Unlike these,  
12 ours does not require a controlled-lighting environment. The results of  
13 the exams can be sent to doctors and patients by instant messaging or  
14 making them available on-line;
- 15 • The design of optics and interactive software that allows a small pro-  
16 grammable display at close proximity to the eye to be effectively used  
17 for visual-field evaluation (Section 3). Our solution is the first truly  
18 portable campimeter. Unlike commercially-available perimeters, ours  
19 contains no mechanically moving parts;
- 20 • A fast algorithm for visual field evaluation that obtains results compa-  
21 rable to the ones used in commercially-available campimeters, both in  
22 terms of quality and examination time (Section 3.3).

## 2. Background and Related Work

Some of the first methods used to evaluate the visual field were the Am-  
sler Grid and the tangent screen [5, 6]. The first perimeter using a cupola  
shape, as used by commercial devices today, was designed by Goldmann in  
1945. Fankhauser developed the first prototype of an automated perimeter in  
1972 [3]. Since then, more sophisticated and precise devices and algorithms  
have been developed.

A modern campimeter works by projecting a series of white light stim-  
uli of various intensities (brightness) across a uniformly illuminated cupola  
(background) that covers the patient’s field of view. Covering one eye at  
a time with an eye patch, the patient looks at a central fixation point and  
indicates (by pressing a button) whether each stimulus is perceived. The  
goal of the exam is to determine the minimum perceived intensities at a set  
of sampling positions across the visual field. The estimated values are pre-  
sented in decibels (dB), computed relatively to the intensity of the uniformly  
illuminated background.

Commercial perimeters are very similar both in shape and functional-  
ity. Currently, some of the most popular campimeters in the market are the  
Humphrey Field Analyzer (HFA) II-i series, manufactured by Zeiss [7], and  
the Octopus 900, manufactured by Haag-Streit [8]. They consist of a com-  
puter together with a mechanical, an electronic, and an optical sub-systems,  
making them heavy, big, expensive machines. For instance, the HFA II-i  
weights 40 Kg, occupying a volume of  $60 \times 58 \times 51$  cm<sup>3</sup> [9], and costing tens  
of thousands of dollars. Carvalho et al. [10] have developed an automated  
campimeter with features similar to the commercially-available campimeters.

1 All these devices require a controlled-lighting environment for operation. In  
2 contrast, our mobile campimeter provides a truly portable, low-cost alterna-  
3 tive for visual-field evaluation. Our co-design of optics and interactive soft-  
4 ware allows the use of a programmable display at close proximity, avoiding  
5 the need for controlled-lighting environment or mechanically moving parts.

6 Tafaj et al. [11] describe a PC-based solution inspired by a mechanical  
7 campimeter developed by Bruckmann et al. [12]. The evaluation of Tafaj  
8 et al.'s campimeter consisted in comparing its measurements of blind-spot  
9 sizes with the corresponding measurements obtained with an Octopus 101  
10 perimeter. No evaluation of the minimum perceived intensities across the  
11 visual field has been provided [11].

12 In recent years, several works [13, 14, 15, 16] have evaluated the use of  
13 tablets (iPads) and apps to perform perimetry. In all these experiments, the  
14 tablet was kept at approximately 33 centimeters from the subject. During the  
15 test, the distance and positioning of the subject with respect to the device are  
16 checked by the tester through visual inspection. The use of tablets required  
17 a controlled-lighting environment and the tests were restricted to up to eight  
18 intensity values. Except for [13], these experiments used fixation points at  
19 the tablet's border, restricting the portion of the visual field that could be  
20 tested at once.

### 21 *2.1. Head-Mounted-Display-based Solutions*

22 Matsumoto et al. [17] and Dariusz et al. [18] developed customized head-  
23 mounted displays (HMDs) for evaluating the visual field. Both HMDs use  
24 high-definition LCD displays and include additional hardware to provide eye-  
25 tracking. The equipment described by Matsumoto et al. [17] includes a so-

phisticated optical system consisting of several components. In both devices, 1  
the field evaluation is controlled by external processing units. Matsumoto et 2  
al. use a tablet to control the test and collect the patient’s responses. The 3  
equipment described by Dariusz et al. is connected by cable to a personal 4  
computer through some customized hardware interface. Unlike these devices, 5  
our mobile campimeter uses a smartphone to control the field evaluation and 6  
collect the patient’s responses, providing a low-cost, autonomous, portable 7  
solution. 8

### 2.2. Smartphone-based Eye Care Solutions 9

Some researchers have proposed eye-care solutions based on smartphones. 10  
NETRA [19] describes an interactive solution for estimating refractive errors 11  
of the human eye (*e.g.*, myopia, hyperopia, and astigmatism). CATRA [20] 12  
provides a system for measuring and mapping cataracts. D-EYE [21] uses 13  
the smartphone camera and light source to allow retinal screening. The 14  
Portable Eye Examination Kit (PEEK) [22] uses apps to identify individuals 15  
with visual impairment. While these projects share several goals with ours 16  
(*e.g.*, portability, low cost, and potential to reach remote and underprivileged 17  
regions of the globe), we focus on campimetry, another important exam. 18

### 2.3. Algorithms 19

Campimetry requires sampling the patient’s field of view. Given the 20  
nature of the test, the patient’s responses need to be double-checked to avoid 21  
incorrect feedback due to distraction or fatigue. This tends to make the test 22  
longer and, in turn, prone to more errors. Thus, a fast and reliable sampling 23  
strategy is highly desirable. SITA Fast [23] is the most popular algorithm 24

1 used in commercial campimeters. It uses a simple staircase strategy, but its  
2 performance relies on the availability of a proprietary database containing  
3 statistical data about the population collected in previous exams over the  
4 years. Our field-of-view sampling algorithm (Section 3.3), although not based  
5 on a large database, has performance similar to the ones used by commercial  
6 campimeters.

### 7 **3. Mobile Campimeter Design**

8 Similar to commercial perimeters, our mobile campimeter estimates the  
9 minimum intensity visible by the patient at a set of sampling positions across  
10 the visual field. It consists of a virtual-reality-like headset driven by a smart-  
11 phone. The psychophysical test is performed through an interactive app.  
12 The stimuli are presented (one at a time) on the smartphone’s screen while  
13 the subject looks at a fixation point at the center of the field of view for the  
14 tested eye. During the test, an eye patch keeps the other eye closed. Next,  
15 we present the details of the hardware and software components of our mo-  
16 bile campimeter. We start by introducing a sampling grid (Section 3.1) for  
17 assessing the sensitivity of one’s visual field to luminous stimuli. Section 3.2  
18 discusses the hardware design and the associated goals and constraints that  
19 shaped our decisions. Our algorithm for evaluating the minimum perceived  
20 intensities across the patient’s visual field is presented in Section 3.3. Sec-  
21 tion 3.4 describes how the results obtained with our mobile campimeter are  
22 scaled to the same decibel range used by commercial perimeters.



### 3.1. The Sampling Grid

The grid of sampling positions (white dots) and the fixation point are shown in Fig. 2 (top). The fixation point is displayed as a red dot and kept on for the entire evaluation. During a visual field evaluation, the stimulus at each sampling position is rendered as a small circle of radius 2 pixels, using OpenGL ES [24] point primitive (`GL_POINT` with `glPointSize(2.0)` and `glEnable(GL_POINT_SMOOTH)`). Given the field of view covered by the smartphone screen (see Sec 3.2 - Headset Design), this corresponds to a 0.43 degree Goldmann size III stimulus, which is the standard size used in automated perimetry [25]. The background intensity of our current prototype corresponds to 18% of the maximum intensity of the smartphone. Although this value was chosen empirically, the Zone System in photography and some tone mapping algorithms often map middle-gray to 18% of the available dynamic range [26]. For each stimulus, the subject indicates whether it has been perceived by pressing a button on a bluetooth device (*e.g.*, a gamepad or a remote control - Fig. 3(f)) paired to the smartphone.

### 3.2. Hardware Design

The hardware development included photometric measurements and the headset design. The first consisted in converting the absolute stimulus intensities displayed by the smartphone's screen to the luminance units used by commercial campimeters. The second describes the headset dimensions and optical system. The smartphone used in our prototype is a Samsung Galaxy S III running Android (Fig. 2).

**Photometric Measurements:** The intensity  $d_c$  of a pixel in the smart-

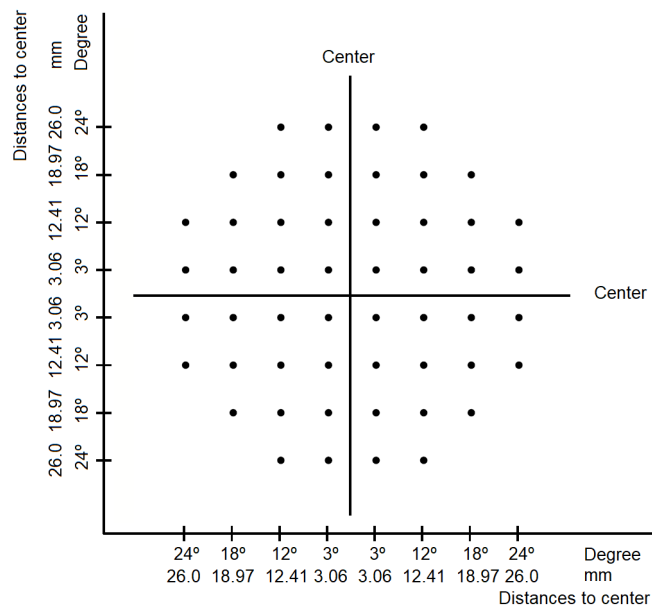
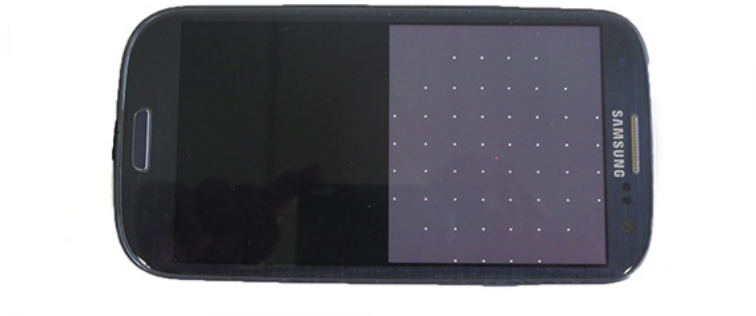


Figure 2: Smartphone (Samsung Galaxy S III) showing the grid of sampling positions (white dots) that cover the field of view for the right eye. The left eye is similar. The fixation point is shown as a red dot at the center of the field. The grid will appear centered to the patient when seen through the headset. The background intensity for the tested eye corresponds to 18% of the display's maximum intensity - compare it to the left part of the display. (bottom) Horizontal and vertical angles and coordinates associated with the sampling positions, expressed with respect to the fixation point.

phone’s screen is specified in the normalized range  $0 \leq d_c \leq 1$ . Commercial 1  
campimeters adopt *apostilb* (*asb*) as their unit of luminance. For compat- 2  
ibility and to allow direct comparison of our results with the ones obtained 3  
with commercial devices, we convert the  $[0, 1]$   $d_c$  range to apostilbs. To ob- 4  
tain such a conversion, we first measured the illuminance (expressed in *lux*, 5  
 $lx = lm/m^2$ ) produced by the smartphone’s screen for one hundred  $d_c$  inten- 6  
sity values (uniformly sampled at 0.01 intervals) using a Minipa MLM-1020 7  
luximeter [27]. We then converted the obtained lux values to apostilbs. The 8  
details of this conversion process are presented in Appendix A. 9

The background intensity on Humphrey perimeters is 31.5 asb or 10.0 10  
 $cd/m^2$ . For our near-eye prototype, we used a background intensity of 11  
3.45 asb or 1.01  $cd/m^2$ . 12

**Headset Design:** Although loss of visual field due to glaucoma can oc- 13  
cur anywhere in the visual field, in most patients detectable loss can be 14  
found in the 24-30° from the center [28]. Typically, evaluations performed 15  
by commercially-available campimeters cover approximately 48 degrees in 16  
the central field of view of each eye (*e.g.*, the HFA II-i evaluates 24 degrees 17  
temporally and 30 degrees nasally, for a total of 54 degrees). Other angular 18  
ranges are used only when some anomaly is detected in this test [25]. Our 19  
goal is to produce a smartphone-based compact device that covers 48 degrees 20  
in the central field of view, horizontally and vertically, for both eyes. 21

The screen of the smartphone used in our prototype is approximately 22  
10.8 cm wide, and half of it should cover each eye (Fig. 2). Thus, the dis- 23  
tance between the most external sampling position and the fixation point 24  
is approximately 2.6 cm. To subtend an angle of 48° for each eye, the dis- 25

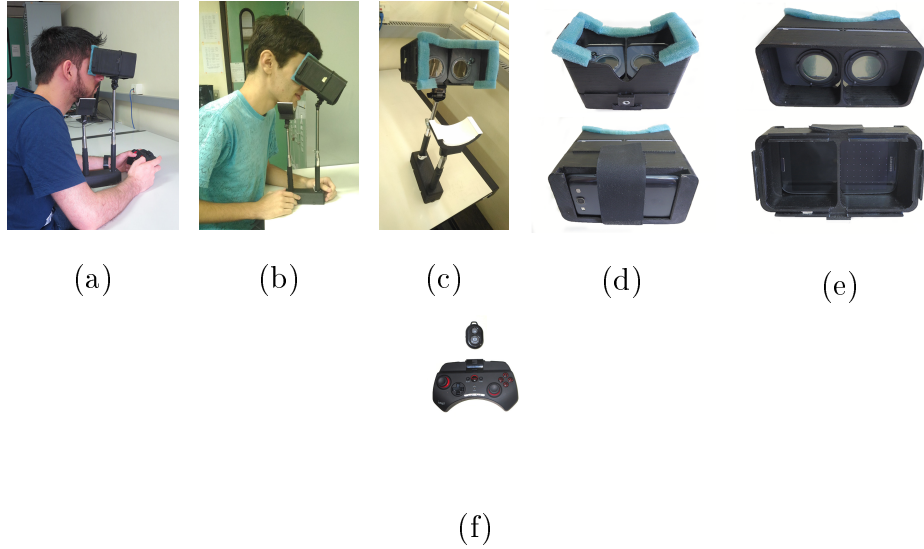


Figure 3: Our mobile campimeter and its components. (a-b) Prototype during a visual field evaluation. The adjustable support for the headset and chin lends to comfortable experiences by different subjects. (c) A view of the prototype with telescopic supports. (d) External views of the prototype: front (top) and back (bottom). (e) Internal views: lenses (top) and smartphone screen (bottom). (f) Bluetooth devices.

1 tance between the eye to the smartphone’s screen (the object) should be

$$2 \quad d = \frac{2.6}{\tan(24^\circ)} \approx 5.84 \text{ cm.}$$

3     The closest distance onto which an (average) individual with normal vi-  
 4 sion is able to focus is 25 cm [29]. This distance is called the *near point* (aka  
 5 *distance of most distinct vision*). Thus, we use a magnifier (*i.e.*, a positive  
 6 lens) to allow the observer to focus on a virtual image of the smartphone’s  
 7 screen [29]. Note that this would preserve the  $48^\circ$  field of view, despite of the  
 8 resulting magnification. The actual distance from the smartphone’s screen  
 9 to the optical system in our current 3D-printed prototype is  $d = 6.50$  cm.  
 10 The focal distance  $f$  for a magnifier at distance  $d$  from the object is given

by [29]:

$$\frac{1}{f} = \frac{1}{d} - \frac{1}{25}, \quad (1)$$

where 25 cm is the near point. For  $d = 6.50$  cm, this implies a magnifier with 11.4 diopters ( $f \approx 8.78$  cm). Since the highest optical power that our lens manufacturer could produce for an aspherical lens was 10.0 diopters, we built an aspherical optical system consisting of two lenses: a 2 diopters lens ( $f_1 = 50$  cm) in front of a 10 diopters one ( $f_2 = 10$  cm), spaced by  $s = 0.5$  cm. The effective focal distance  $f'$  of the resulting optical system is given by [30]:

$$\frac{1}{f'} = \frac{1}{f_1} + \frac{1}{f_2} - \frac{s}{f_1 f_2}, \quad (2)$$

which results in an optical power of 11.9 diopters ( $f' = 8.40$  cm). In a preliminary evaluation of our prototype, subjects reported that they could comfortably focus at the (virtual) image of the smartphone's screen.

Measured with respect to the fixation point, the sampling positions are at  $3^\circ$ ,  $12^\circ$ ,  $18^\circ$ , and  $24^\circ$  at both sides of the horizontal and vertical fields of view (*i.e.*, from  $-24^\circ$  to  $24^\circ$ , at  $6^\circ$  intervals - Fig. 2 (bottom)). Since we use a flat screen, this translates into a non-uniform linear spacing among the sampling positions. Given the display-lens distance  $d$  and considering the fixation point at the origin, the horizontal (vertical) coordinate of a sampling point making an angle of  $\alpha$  degrees with the visual axis is given by  $c = d \tan(\alpha)$ . Thus, for the theoretical distance  $d = 5.84$  cm and for angles of  $3^\circ$ ,  $12^\circ$ ,  $18^\circ$ , and  $24^\circ$ , the coordinates are respectively, 3.06 mm, 12.41 mm, 18.97 mm, and 26.00 mm away from the corresponding coordinate of the fixation point, both horizontally and vertically (Fig. 2 (bottom)). Since our current prototype has  $d = 6.5$  cm, these sampling positions cover  $21.8^\circ$  in-

1   stead of  $24^\circ$ . Improvements in the 3D printing and assembly of the prototype  
2   should remove such small discrepancy.

3       The headset was designed using the software SolidWorks [31] and pro-  
4   duced on a 3D printer. It consists of two main parts: a frontal one, which  
5   contains the optical system (Fig. 3(e - top)); and a back part that houses  
6   the smartphone (Fig. 3(e - bottom)). The headset has a (removable) tele-  
7   scopic support for adjusting the height and orientation of the device to the  
8   patient-furniture arrangement. It also has an adjustable telescopic chin rest  
9   (Fig. 3(a)-(c)). Fig. 3 (a) and (b) show two individuals with different heights  
10  using our prototype. Note how the ability to adjust the heights of the  
11  telescopic supports as well as the orientation of the headset allows for cus-  
12  tomized experiences for different patients. Once detached from its support,  
13  the headset can be used by patients laying in beds. A bluetooth input de-  
14  vice (Fig. 3(f)) paired to the smartphone is used to provide user feedback,  
15  informing that the current stimulus has been perceived by the patient. Some  
16  cushioning (blue sponge in Fig. 3) provides comfortable contact and helps to  
17  block ambient light.

### 18   3.3. *Estimating the Minimum Perceived Intensities*

19       We have developed a binary-search-based algorithm for evaluating the  
20  minimum perceived intensities across the patient’s visual field. In general,  
21  the minimum intensities perceived by an individual tend to be similar to the  
22  population-average minimum perceived values for the same positions. Our  
23  algorithm exploits this fact to accelerate convergence by starting the search  
24  near the population average. However, the actual result of the exam is not  
25  affected by the availability of such data. Similar to commercial campimeters,

we also use the population-average values to position the patient with respect  
to the population results.

Let  $F$  be the 2-D grid of sampling positions across the visual field (Fig. 2  
and Fig. 4 (top left)). Given the left (or right) eye, its blind spot  $b$  falls in  
a known neighborhood  $B$  in  $F$ . During the evaluation of the visual field,  
the stimuli are randomly shown at positions across the grid  $F$  for which the  
minimum intensities still need to be determined. The evaluation starts by  
detecting the blind spot. Thus, in the beginning of the examination, the cho-  
sen positions should alternate between inside and outside the neighborhood  
 $B$  until the position of  $b$  has been determined. The blind spot is defined as  
the grid position in  $B$  with the largest number of patient misses. Once the  
position of the blind spot has been determined, the test proceeds until all  
positions in  $F$  have their corresponding minimum perceived intensities esti-  
mated. The minimum intensity of a sampling position is determined when  
the difference between its maximum and minimum perceived intensities is  
less than a threshold (0.03 in the  $[0, 1]$   $d_c$  range).

The minimum perceived intensity values vary across the visual field (Fig. 4  
(left)). In order to quickly estimate the minimum perceived intensity at a  
sampling position  $p_i$ , we use a binary search. The initial intensity test value  
is set to  $d_{ini} = 1.25 \times pm_i$  (converted to the smartphone's  $[0, 1]$  intensity  
scale), where  $pm_i$  is the population-average minimum perceived intensity at  
 $p_i$ . The lower boundary of the search interval is set to  $d_{lower} = 0.19$ , which is  
the first intensity above the background intensity ( $d_{bkg} = 0.18$ ). The upper  
boundary is set to  $d_{upper} = 1.0$ . Given such initial and boundary values, the  
estimate of the minimum perceived intensity is obtained with the following

1 procedure: if the patient perceives the stimulus with intensity  $d_{ini}$ , then the  
2 algorithm performs a binary search in the interval  $[d_{lower}, d_{ini}]$ ; otherwise, it  
3 performs a binary search in the interval  $[d_{ini}, d_{upper}]$ . During the test, the  
4 system occasionally presents a stimulus at the location of the detected blind  
5 spot to double check if the patient has preserved the original head alignment.

6 The minimum reaction time for humans is 180 ms [32]. As such, we con-  
7 sider any patient’s response below 180 ms as a false positive. Each stimulus  
8 is shown for 200 ms and the system waits additional 800 ms for the patient’s  
9 answer. Thus, a new stimulus is shown every second. SITA Fast also uses a  
10 fixed time interval between consecutive stimuli [23, 32].

### 11 3.4. Dynamic Range

12 The HFA II-i campimeter can generate light stimuli with brightness  
13 varying from 0.08 asb up to 10,000 asb [25]. Since such stimuli are projected  
14 onto a uniformly illuminated background, its full brightness range can, the-  
15 oretically, be exploited. According to our measurements (Section 3.2 - Pho-  
16 tometric Measurements), the brightness of the stimuli that can be displayed  
17 on the screen of the smartphone used to build our prototype varies from 0.13  
18 asb up to 168.46 asb. Since its background intensity is set to 3.45 asb or 1.01  
19  $cd/m^2$  (Fig. 2), the actual intensity range available for examination varies  
20 from 4.24 asb ( $1.35 cd/m^2$ ) to 168.46 asb ( $53.62 cd/m^2$ ). This corresponds  
21 to a maximum decibel value of  $Max\_dB_{prot} = 10 \log(168.46/4.24) \approx 16$  dB.  
22 The HFA II-i, in turn, can reach a maximum decibel value of  $Max\_dB_{HFA} =$   
23  $10 \log(10,000/0.08) \approx 51$  dB. However, the upper 11 dB of the stimulus range  
24 (*i.e.*, from 41 to 51 dB) results from very dim stimuli, which fall beyond  
25 the range of human vision under standard testing conditions [25]. Thus,



for practical purposes  $Max\_dB_{HFA} = 40$  dB, which gives us a factor of  $Max\_dB_{HFA}/Max\_dB_{prot} = 2.5$ .

To produce reports that can be directly compared to the ones of commercial campimeters and allow doctors to interpret them in the same way, we scale the dB values estimated with our prototype to the range of the HFA II-i. For this, we performed a simple experiment to estimate a per-sampling-position scaling factor. We had six volunteers to perform a field examination for each eye on both devices. Note that some of these volunteers did not take part in the user study described in Section 4. For each eye, and for each sampling grid position  $p_i$ , we computed a corresponding scaling factor  $s_i$  as the average of the ratios of the corresponding values in the two exams for the same subject/eye (Eq. (3)):

$$s_i = \frac{1}{n} \sum_{j=1}^n (h_{ji}/m_{ji}), \quad (3)$$

where  $h_{ji}$  and  $m_{ji}$  are, respectively, the minimum intensity values (in dB) for the sampling position  $p_i$  in the HFA II-i and in our mobile campimeter reports for the  $j$ -th subject. For the results shown in the paper, we used  $n = 6$ , although a larger number would be desirable, given the variability observed even when repeating the evaluation of a given subject/eye on the same device. Fig. 5 shows the estimated scaling factors for each visual-field sampling position on the right eye. Note that they are all close to the predicted 2.5 factor, with the largest values close to the blind spot. Fig. 4 (top) shows examples of reports generated by our prototype. The numbers are in decibels (dB), with the blind spot exhibiting a value of zero. In the graphical representation on the right, the blind spot is shown as a black

1 region. For comparison, the corresponding reports produced by the HFA II-i  
2 for the same subject/eye are shown in Fig. 4 (bottom). An example of a  
3 complete report generated by our mobile campimeter is shown in Appendix  
4 B.

#### 5 **4. User Study and Results**

6 To validate our mobile campimeter prototype and evaluate its perfor-  
7 mance relative to the Humphrey HFA II-i, we performed a user study in-  
8 volving a group of 20 volunteers with normal or corrected to normal vision.  
9 These included 17 males (ages 24 to 31), and 3 females (ages 23 to 27).  
10 Each subject performed two visual field examinations (test and retest) using  
11 both the Humphrey HFA II-i perimeter and our mobile campimeter proto-  
12 type. This non-invasive user study was approved by the Federal University  
13 of Rio Grande do Sul (UFRGS) Medical Ethics Committee (document num-  
14 ber 1.652.293). The HFA II-i perimeter used in this research is registered  
15 under number 10332030093 at the National Agency for Health Surveillance  
16 (ANVISA) in Brazil. The exams using the Humphrey perimeter were carried  
17 out at an ophthalmology center (CORS).

18 Some volunteers had their visual field evaluation performed first on the  
19 HFA II-i and then on our prototype, while the remaining had their evaluation  
20 first on the prototype and then on the HFA II-i. All volunteers had their  
21 examinations over a period of two days. In each day, two evaluations (test  
22 and retest) were done with the same device, with a twenty-minute interval  
23 between the tests. This way, the tests on a given device did not influence  
24 the results of tests on the other equipment. The retest was intended to check

the repeatability of the evaluation on each device and to detect problems 1  
due to distractions during the evaluation. From a total of 40 evaluations, 2  
the average evaluation time was 2 minutes and 50 seconds on the HFA II-i 3  
using SITA Fast, and 3 minutes and 26 seconds on our prototype using the 4  
algorithm described in Section 3.3. 5

We performed a detailed analysis of the evaluation results. These include 6  
separate scores for each volunteer’s eye in each device, comparison of the 7  
subjects’ results obtained in both devices, and comparison of the subjects’ 8  
results against the (estimated) population means. In each case, the compar- 9  
isons considered the individual sampling positions across the visual field. For 10  
this analysis, we also use statistical indices proposed by [4], which include 11  
*mean deviation*, *pattern standard deviation* (Fig. 6), as well as a reproducibil- 12  
ity evaluation (Fig. 8) based on the method by [33]. 13

#### 4.1. Mean Deviation 14

The *mean deviation* (MD) index is a weighted average deviation from 15  
the normal reference field. It is used to detect regions in the visual field 16  
that present minimum intensity values significantly different from an average 17  
normal field. It is computed as 18

$$MD = \left( \frac{1}{N} \sum_{i=1}^N \frac{(v_i - \mu_i)}{\sigma_i^2} \right) / \left( \frac{1}{N} \sum_{i=1}^N \frac{1}{\sigma_i^2} \right), \quad (4)$$

where  $v_i$ ,  $\mu_i$ , and  $\sigma_i^2$  are, respectively, the estimated minimum intensity value, 19  
the population minimum intensity average, and the population minimum 20  
intensity variance for sampling position  $p_i$ .  $N$  is the number of sampling 21  
positions in the visual field, excluding the blind spot. 22

1 The graph on the left of Fig. 6 compares the mean deviation computed  
2 for our prototype and for the HFA II-i perimeter. The 40 points in the graph  
3 show the average of test and retest for 20 volunteers considering the left and  
4 the right eyes. Note that, although the average mean deviation is smaller  
5 for the HFA II-i, the values vary consistently in both devices: when the MD  
6 index computed for the HFA decreased/increased from one subject/eye to  
7 another, a similar variation was observed for the MD index computed for our  
8 prototype. The MD indexes shown in Fig. 6 (left) have a Pearson correlation  
9 coefficient of 0.754, indicating a strong agreement.

#### 10 4.2. Pattern Standard Deviation

11 The *pattern standard deviation* (PSD) index is the weighted standard  
12 deviation on each point between the measured intensity and the normal ref-  
13 erence field. We check how far the measured value for this point is from  
14 its average and from the mean deviation. A small PSD value indicates that  
15 the measured values are close to the normal reference field, whereas a big  
16 PSD value indicates one or more regions with a big difference to the normal  
17 reference field. The PSD index is computed with Eq. (5). The graph on the  
18 right of Fig. 6 compares the PSD values computed for our prototype and for  
19 the HFA II-i perimeter, considering the evaluations performed in the user  
20 study. The Pearson correlation coefficient for the values in the two curves is  
21 0.4, indicating a weak-to-moderate agreement.

$$PSD^2 = \frac{1}{N} \sum_{i=1}^N \sigma_i^2 \frac{1}{N-1} \sum_{i=1}^N \frac{(v_i - \mu_i - MD)^2}{\sigma_i^2}. \quad (5)$$



1 the prototype is slightly smaller than the one for the HFA II-i: 2.16 dB for  
 2 the prototype and 2.38 dB for the HFA II. Appendix B provides a detailed  
 3 comparison of the results for the test and retest for each subject/eye on both  
 4 devices.

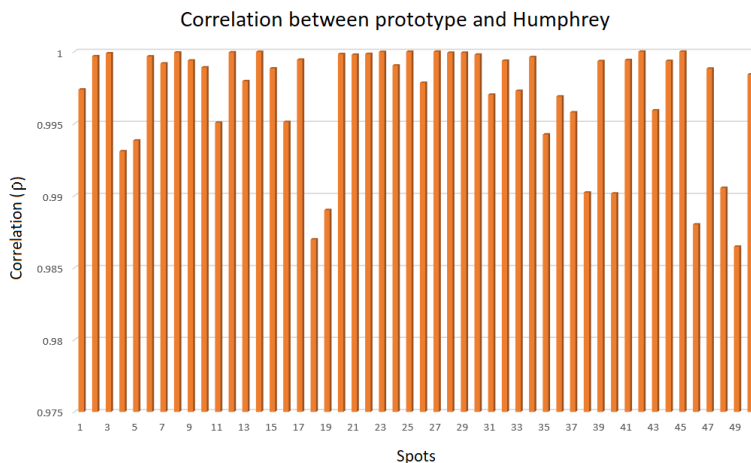


Figure 9: Pearson correlation coefficient  $\rho$  between the minimum intensity values estimated by our prototype and the HFA II-i for each of the 50 sampling positions in the visual field.

#### 5 4.4. Pearson Correlation between Devices

6 We computed the Pearson correlation coefficient  $\rho$  between the minimum  
 7 intensity values estimated by our prototype and by the HFA II-i for each of  
 8 the 50 sampling positions in the visual field (Fig. 9). The results show a very  
 9 strong correlation, with  $\rho > 0.98$  for all sampling positions.

#### 10 4.5. Discussion

11 Campimetry is an exam that requires the patient’s total attention for a  
 12 few minutes. Thus, it is important to allow her/him to be comfortable during  
 13 the examination, avoiding lack of attention due to tiredness. For this, we have

designed our mobile campimeter with adjustable supports for the headset and 1  
for the chin (Figures3 (a-b)). While a large variety of virtual-reality glasses 2  
are available on the market, they were designed for a different purpose, and do 3  
not provide this kind of feature. Moreover, to use the full display resolution 4  
for the desired field-of-view ( $48^\circ$  per eye), we designed a headset with a bigger 5  
distance from its optical system to the smartphone screen (approximately 2 6  
cm longer) than the typical distance found in commercially available virtual- 7  
reality glasses. Designing our own headset gave us more flexibility in our 8  
project decisions. 9

For our current prototype, we divided the smartphone's canonical  $([0,1])$  10  
intensity interval into 100 steps of 0.01. As the device's maximum intensity 11  
increases, the size of the quantization step can be reduced, making the mea- 12  
surements more precise. However, since it is unlikely that the dynamic range 13  
of smartphones matches the one of commercial campimeters anytime soon, 14  
a scaling procedure such as the one described in Section 3.4 should still be 15  
required. 16

The use of an eye tracker could help to detect the situations in which the 17  
patient is looking away from the fixation point. This, however, has implica- 18  
tions in terms of cost and size, and is hard to integrate with a smartphone. 19  
Like most commercial devices, we avoid the need for an eye tracker by peri- 20  
odically testing the blind spot location. 21

The calibration measurements (see Appendix A) used disks (of variable 22  
radii) shown under the luximeter's sensor. As a small disk moves away from 23  
the fixation point, one should expect an intensity falloff by the cosine of the 24  
angle  $\angle ABC$  formed by the fixation point (A), the eye position (B), and the 25

1 center of the grid point (C) where the disk is located. For a centered 48°  
2 field-of-view, the maximum angle of a ray with the viewing direction is 24°,  
3 whose cosine is 0.913. Thus, the maximum intensity loss is under 10% and  
4 did not seem to have had any relevant impact on the visual field evaluation.

5 Our current prototype has a fixed interpupillary distance - IPD (6.2 cm).  
6 This decision was intended to simplify the design and construction of the  
7 prototype. However, this does not seem to affect the actual visual field  
8 examination, as perimetry is performed with a single eye opened at a time.

9 We emphasize that the goal of our mobile campimeter is not to replace  
10 commercial devices or ophthalmologists. It provides a portable and accessible  
11 alternative for screening patients, identifying the ones who need more careful  
12 examination, with the potential to reach remote and underprivileged areas.

#### 13 4.6. Limitations

14 The lenses used in our prototype have a diameter of 37.5 mm, causing the  
15 patient to look at the smartphone's screen through a circular window with  
16 a 34-millimeter diameter. Misalignments of the patient's eye with respect  
17 to such a window may happen during the evaluation, leading to occlusion  
18 of sampling points located at the borders of the visual field, affecting the  
19 estimated minimum intensity values at such positions. Fig. 10 illustrates  
20 this situation for one of the exams in our user study. Note the existence of  
21 two adjacent sampling positions with 0 dB values. The occurrence of such  
22 an outlier (a *double blind spot*) in healthy subjects results from an improper  
23 positioning of the eye with respect to the headset.



## 5. Conclusion

1

We have demonstrated a portable, low-cost, easy-to-manufacture smartphone-based campimeter. We evaluated our prototype through a user study and compared its results against the ones obtained on a Humphrey HFA II-i, one of the most popular commercially-available perimeters. We have presented detailed comparisons between both devices using several statistical indices. Our analyses have shown that the results obtained with our prototype are consistent with the ones obtained with the HFA II-i campimeter, with a Pearson's correlation coefficient above 0.98 for all sampling positions in the visual field. Moreover, its reproducibility and examination time are also comparable to the ones of the Humphrey campimeter using the SITA Fast algorithm. Despite the use of modest hardware, our results exhibit good approximation to the ones obtained with commercial devices that cost tens of thousands of dollars. Given its true portability and low cost, our mobile campimeter provides a promising alternative for patient screening in schools and community health centers, as well as for visual evaluation of patients with mobility restrictions, for keeping track of the visual field at home, and for use in communities with limited access to medical services. The results of the exams can be sent to doctors and patients by instant messaging or made available on the Internet.

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As future work, we would like to improve the design of our headset to reduce positioning misalignments, and use larger lenses to reduce occlusions of sampling positions at the border of the visual field.

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## 1 Acknowledgments

2 This work was sponsored by CNPq-Brazil (grants and fellowships 423673/2016-  
3 5, 306196/2014-0) and CAPES.

## 4 Appendix A. Conversion of Measured Lux Values do Asb

5 To perform the measurements, we built a black box (its interior covered  
6 with black dull paint) to contain the smartphone at its bottom. The black  
7 box has a circular hole on top for the luximeter's sensor, isolating it from  
8 external light (Figure A.11 (left)). The sensor is located at a distance  $r$  from  
9 the smarthphone's display (we used  $r = 8$  cm). Since  $1 \text{ lx} = 1 \text{ sr cd/m}^2$ , and  
10  $3.14 \text{ asb} = 1 \text{ cd/m}^2$ , we obtain

$$1 \text{ asb} = \frac{1}{3.14} \frac{\text{lx}}{\text{sr}}, \quad (\text{A.1})$$

11 where  $\text{sr}$  (steradian) is a measure of solid angle. Table A.1 shows the values  
12 (in lux) measured by the luximeter for ten  $d_c$  intensities when displaying  
13 circles with radius ranging 5 to 30 mm.

14 The solid angle  $\omega$  subtended by a circle with radius  $R = MP$  displayed  
15 on the smartphone's screen is obtained as  $\omega = A/r^2$ , where  $A$  is the area  
16 of the purple spherical cap shown in Fig. A.11 (right) and  $r$  is the distance  
17 from the center of the sensor to the screen. The area  $A$  of the spherical cap  
18 is given by  $A = 2\pi rh$ , where  $h$  is the height of the spherical cap. By similar  
19 triangles (see Fig. A.11 (right)),  $\frac{MP}{r} = \frac{a}{r-h}$ . Thus,  $h = r\left(1 - \frac{a}{MP}\right)$ .

20 Since  $a = \frac{MP}{OP}r$  and  $OP = \sqrt{(R^2 + r^2)}$ ,  $\omega = 2\pi\left(1 - \frac{r}{\sqrt{(R^2 + r^2)}}\right)$ . Thus,  
21 according to Eq. (A.1), given  $v_L$ , the value in lux measured by the luximeter

Table A.1: Illuminance (in lux) measured by the luximeter for 10 equally-spaced  $d_c$  values and six circular stimulus with radius  $R$  equal to 5, 10, 15, 20, 25, e 30 millimeters.

$d_c$	$R = 5$	$R = 10$	$R = 15$	$R = 20$	$R = 25$	$R = 30$
0.1	0	0.11	0.19	0.26	0.38	0.49
0.2	0.22	0.68	1.44	2.39	3.57	4.78
0.3	0.45	1.63	3.49	5.92	8.77	11.81
0.4	0.83	3.11	6.68	11.2	16.6	22.8
0.5	1.33	4.90	10.45	17.7	26.4	35.6
0.6	1.97	7.52	16.07	27.5	40.5	54.4
0.7	2.81	10.64	23.1	39.1	57.4	76.6
0.8	3.83	14.51	31.6	53.0	77.6	103.4
0.9	5.01	19.00	41.3	69.1	100.9	132.5
1	6.34	20.6	52.5	87.9	129.1	161.3

for a circle with radius  $R$  subtending a solid angle  $\omega$  on the sensor, the value  $v_A$  in apostilbs is given by

$$v_A = \frac{1}{3.14} \frac{v_L}{\omega}. \quad (\text{A.2})$$

## Appendix B. Analysis of Test and Retest Results

This appendix provides detailed comparisons of the results for the test and retest for each subject/eye on both devices. Fig. B.12 compares the RMS error (Eq. (6)) in dB between test and re-test results for each subject/eye.

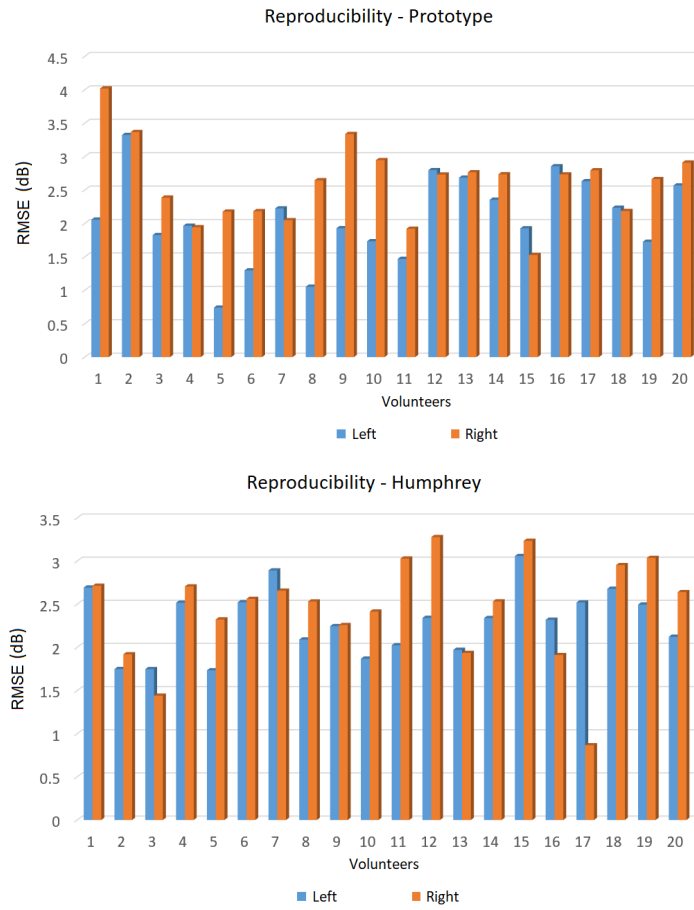


Figure B.12: Reproducibility: RMS error (Eq. (6)) in dB between test and re-test results for each subject/eye. (top) Our prototype. (bottom) HFA II-i.

- 1 Fig. B.13 compares mean deviation indices (Eq. (4)) in dB between test
- 2 and re-test results for each subject/eye.

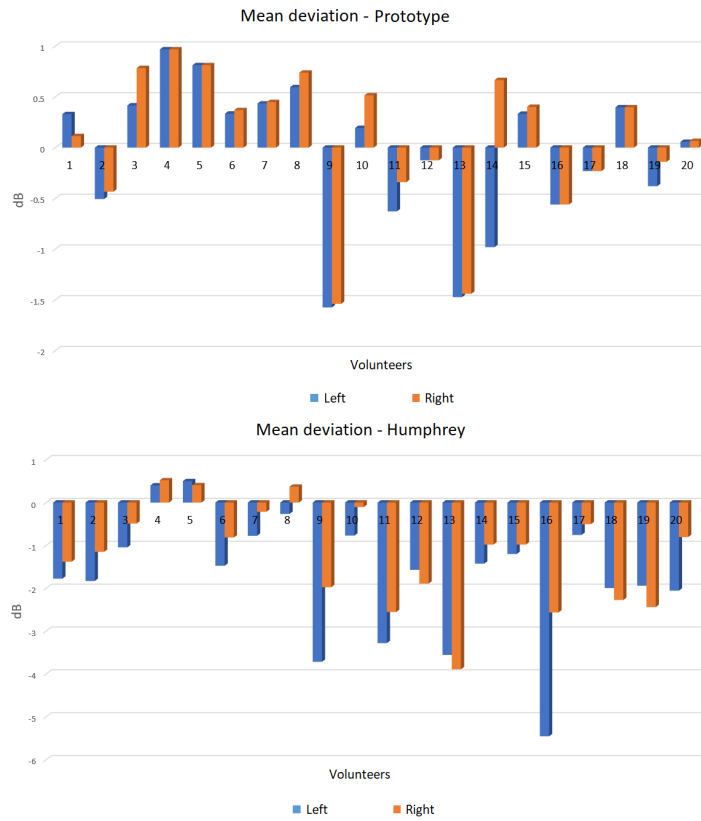


Figure B.13: Mean Deviation computed according to Eq. (4) considering test and re-test results for subject/eye. (top) Our prototype. (bottom) HFA II-i.

Fig. B.14 compares the pattern standard deviation indices (Eq. (5)) in 1  
 dB between test and re-test results for each subject/eye. 2



Figure B.14: Pattern Standard Deviation computed according to Eq. (5) considering test and re-test results for each subject/eye. (top) Our prototype. (bottom) HFA II-i.

## 1 Appendix C. Example of a Complete Evaluation Report

2 Figure C.15 shows an example of a complete evaluation report generated  
 3 by our mobile campimeter. The reports are generated automatically at the  
 4 end of each examination and saved as a PDF file in the smartphone storage.

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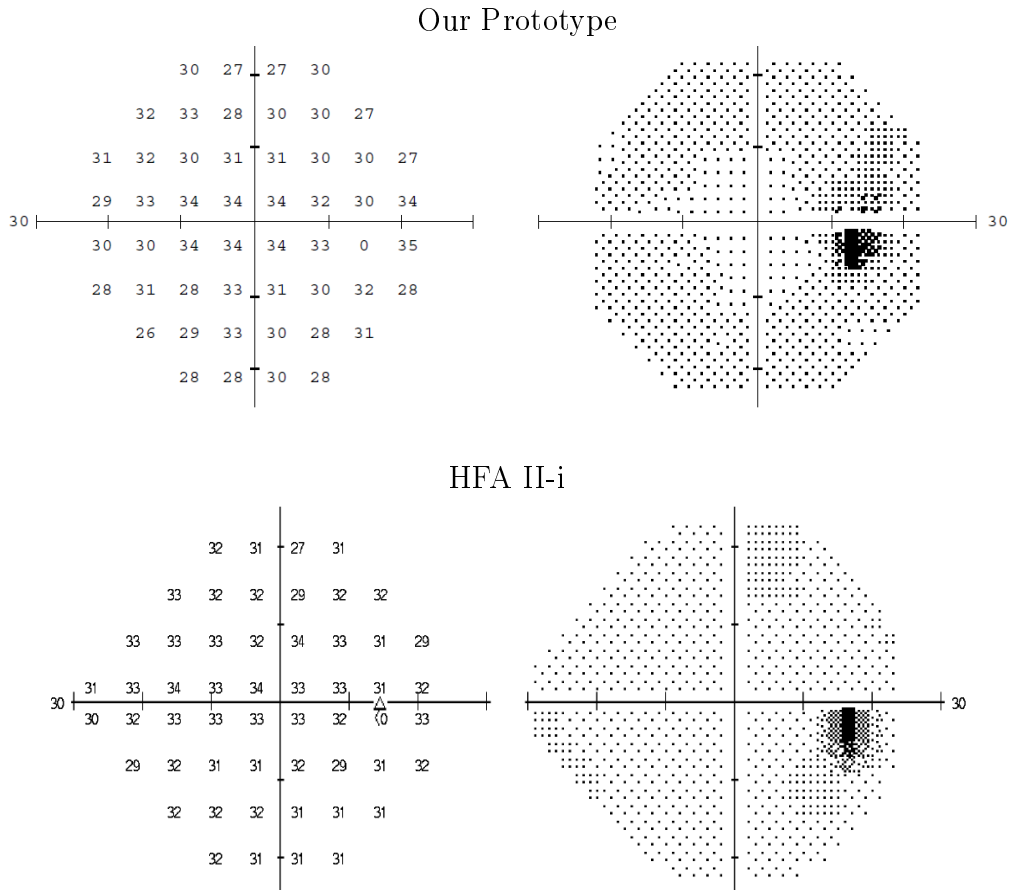


Figure 4: Campimetry reports produced by our prototype (top row) and by the Humphrey HFA II-i (bottom) for the same eye of a given patient. (left) Maps showing the minimum perceived intensity for each sampled point of the visual field, expressed in decibels (dB). (right) Graphical representations of the numerical maps on the left. In each report, the blind spot appears as a black region and corresponds to a value of 0 (zero) dB in the numerical map.

### Scaling Factors

```

2.14 1.93 1.93 2.15
2.29 2.38 2.21 2.31 2.31 2.08
2.13 2.29 2.21 2.07 2.13 2.14 2.31 2.14
2.13 2.20 2.27 2.27 2.27 2.36 2.14 2.46
2.21 2.20 2.27 2.33 2.27 2.20      2.54
2.15 2.38 2.21 2.20 2.13 2.14 2.36 2.00
2.00 2.23 2.21 2.21 2.07 2.13
2.00 2.07 2.14 2.00

```

Figure 5: Scaling factors computed with Eq. (3) for the right eye. They are used to adjust the dB values of the minimum perceived intensities estimated by our prototype to allow a direct comparison with the HFA II-i report.

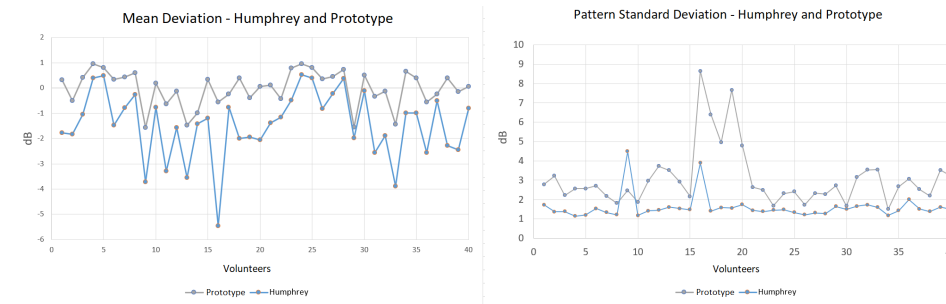


Figure 6: Comparisons between our prototype and the Humphrey perimeter. The 40 points in the graphs show the corresponding index values computed considering the average of test and retest for each eye, for 20 volunteers. (left) Mean deviation (MD). (right) Pattern standard deviation (PSD).

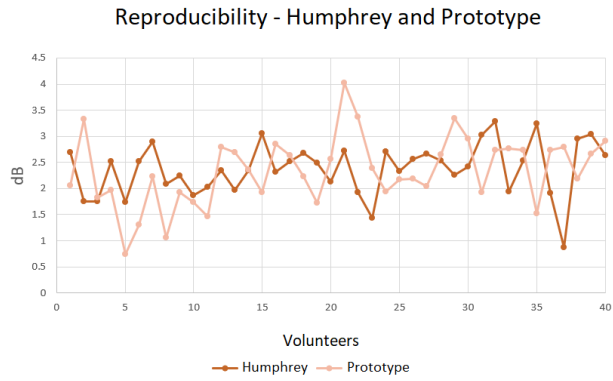


Figure 8: Comparison of the reproducibility between our prototype and the HFA computed as the root mean square error between test and retest for a given subject /eye on the same device.

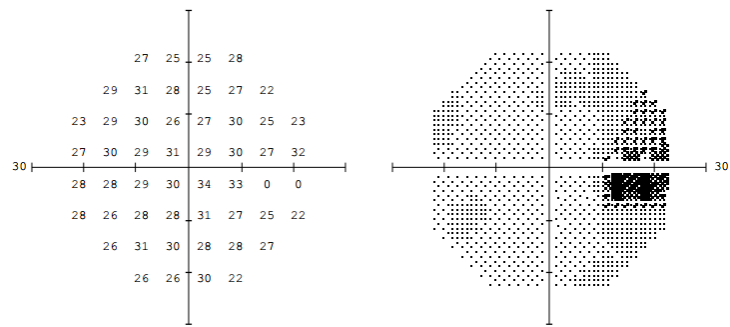


Figure 10: Misalignments of the patient's eye with respect to the headset may lead to occlusion of sampling points located at the borders of the visual field. This example shows a *double blind spot* resulting from misalignment.

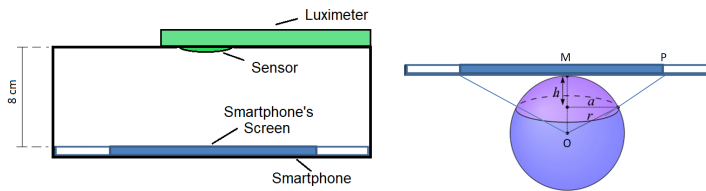


Figure A.11: Phometric measurement. (left) A black box with a circular hole on top for positioning the luximeter's sensor facing the smartphone's screen, placed at a distance  $r$  ( $= 8$ ) cm away at the bottom of the box. The black box isolates the sensor from external light. (right) Geometric configuration for estimating the solid angle subtended by a circle of radius  $MP$  displayed on the smartphone's screen, as perceived by the luximeter's sensor. The sensor is located at the center of the sphere, at a distance  $r$  from the smartphone screen. The solid angle subtended by the circle is obtained dividing the area of the purple spherical cap by  $r^2$ .

Single Field Analysis	Eye: Right
Name: MARCELO DA MATA	Date of birthday: 06/10/1990

Central 24-2 Threshold Test

Fixation target: Central      Stimulus: III, White      Date: 06/04/2016      Time: 16:52  
 Fixation Losses: 1/10      Strategy: Fast Binary Search      Age: 27  
 False POS Errors: 0%  
 False NEG Errors: 0%  
 Test Duration: 03:25

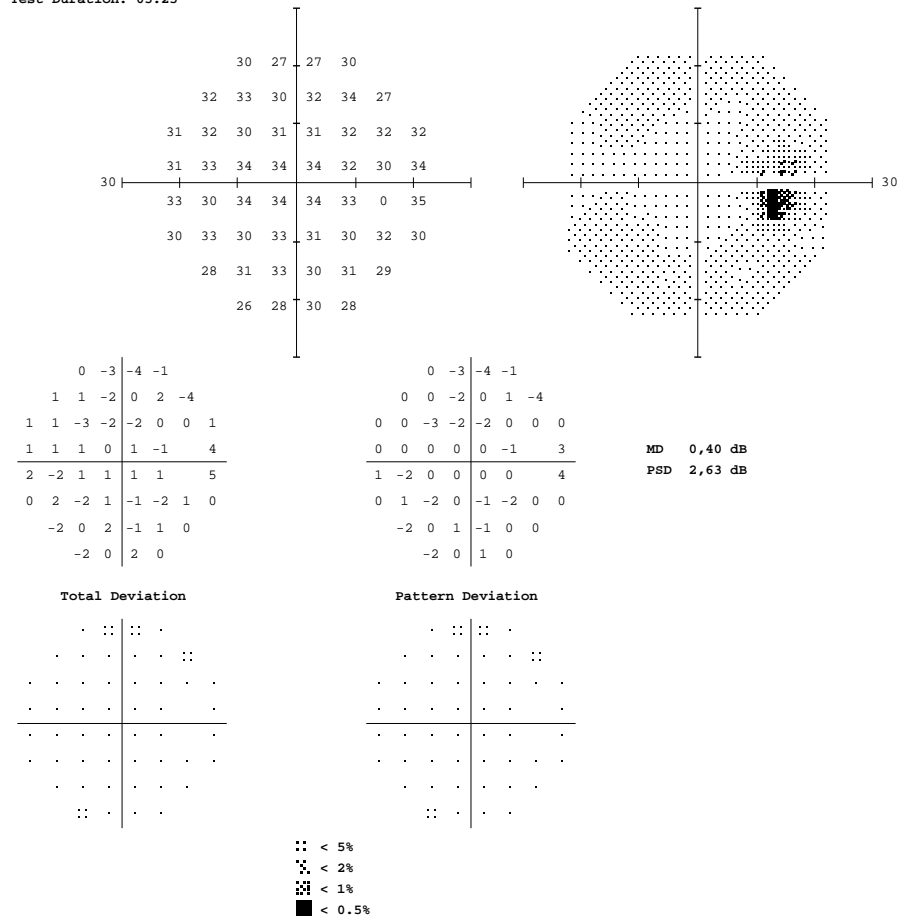


Figure C.15: Example of a full report generated by our mobile campimeter.